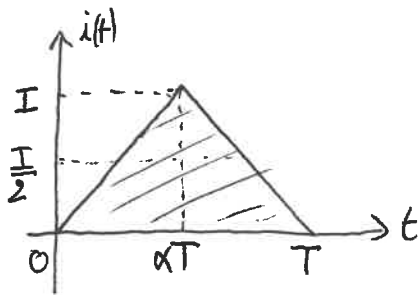
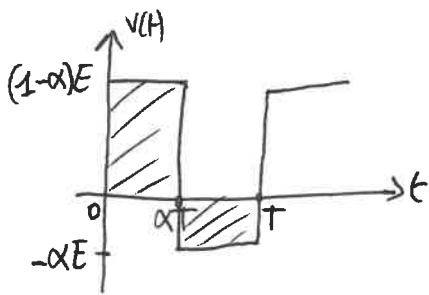


1.)

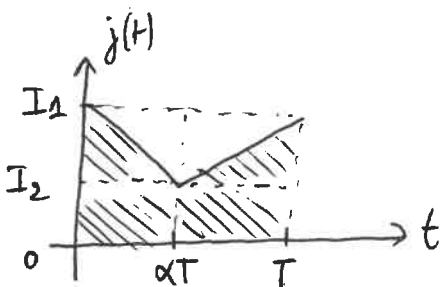
$$i(t) = \begin{cases} \frac{t}{\alpha T} I & \text{si } 0 \leq t < \alpha T \\ \frac{t-T}{\alpha T - T} I & \text{si } \alpha T \leq t < T \end{cases}$$



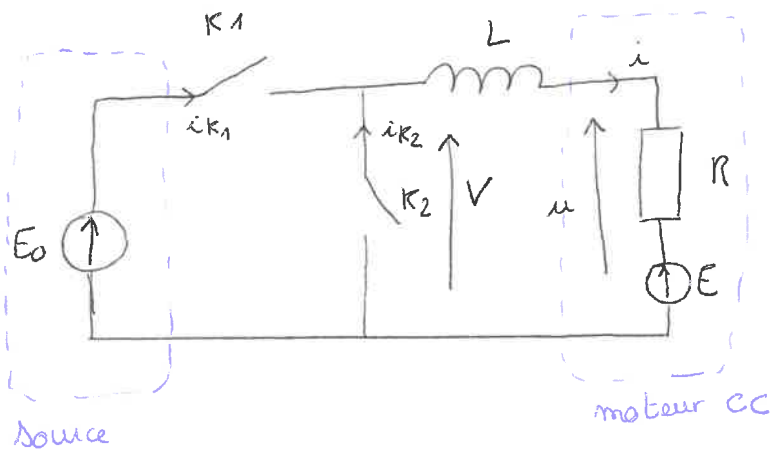
$$\langle i(t) \rangle = \frac{1}{T} \int_0^T i(t) dt = \frac{1}{T} \cdot \frac{I \cdot T}{2} = \frac{I}{2}$$



$$\begin{aligned} \langle v(t) \rangle &= \frac{1}{T} \int_0^T v(t) dt = \frac{1}{T} \left(\int_0^{\alpha T} v(t) dt + \int_{\alpha T}^T v(t) dt \right) \\ &= \frac{1}{T} \left(\alpha T (1-\alpha) E + (T-\alpha T) (-\alpha E) \right) \\ &= \alpha(1-\alpha) E - (1-\alpha)(\alpha E) = 0 \end{aligned}$$

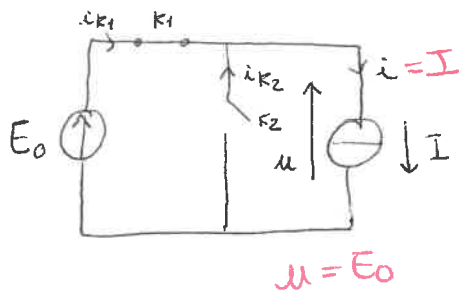


$$\begin{aligned} \langle j(t) \rangle &= \frac{1}{T} \left(\int_0^{\alpha T} j(t) dt + \int_{\alpha T}^T j(t) dt \right) \\ &= \frac{1}{T} \left(I_2 \cdot \alpha T + \left(\frac{I_1 - I_2}{2} \alpha T \right) \right) \\ &\quad + \frac{1}{T} \left(I_2 \cdot (T - \alpha T) + \left(\frac{I_1 - I_2}{2} (T - \alpha T) \right) \right) \\ &= \frac{1}{T} \left(I_2 \alpha T + \frac{(I_1 - I_2) \alpha T}{2} + I_2 (T - \alpha T) + \frac{(I_1 - I_2) (T - \alpha T)}{2} \right) \\ &= I_2 \alpha + \frac{(I_1 - I_2) \alpha}{2} + I_2 (1 - \alpha) + \frac{(I_1 - I_2) (1 - \alpha)}{2} \\ &= \frac{(I_1 - I_2) (\alpha + 1 - \alpha)}{2} + I_2 (\alpha + 1 - \alpha) = \frac{I_1 - I_2}{2} + I_2 = \frac{I_1 + I_2}{2} \end{aligned}$$



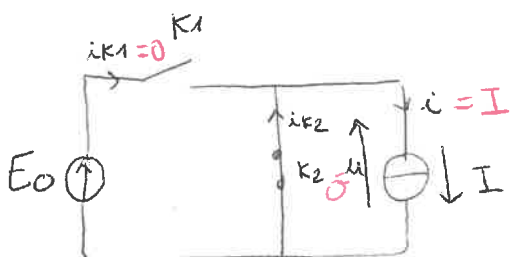
1. Un interrupteur idéal ne consomme pas de puissance
 → les commutations sont instantanées.
2. La bobine L assure la continuité de $i(t)$ et diminue l'amplitude de l'ondulation
 On peut remplacer le moteur CC et la bobine par une source de courant parfaite.

3. * Circuit 1, K_1 fermé et K_2 ouvert



Ce circuit est possible car la source de tension est connectée à une source de courant.

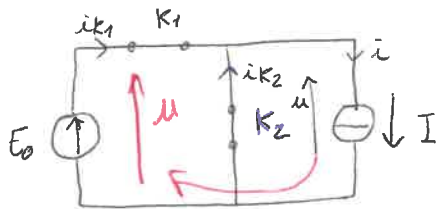
* Circuit 2, K_1 ouvert et K_2 fermé



$i_{K1} = 0$ possible pour une source de tension

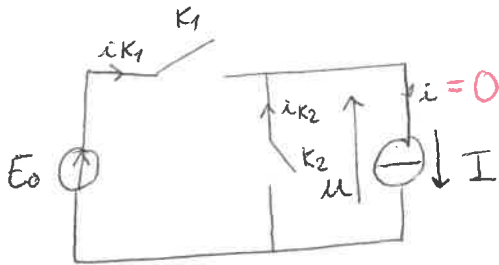
Ce circuit ~~est~~ ~~pas~~ possible car :
 • $u = 0$ qui ~~est~~ ~~pas~~ possible pour une source de ~~tension et~~ ~~current~~
 • $i = I$ qui n'est pas possible pour une source de courant

* Circuit 3, K_1 et K_2 fermés



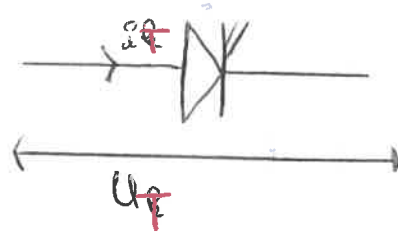
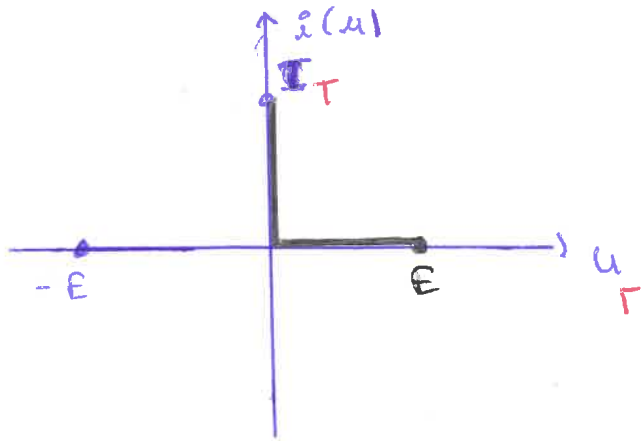
Ce circuit n'est pas possible car $u=0$ qui n'est pas possible pour une source de tension

* Circuit 4, K_1 et K_2 ouverts

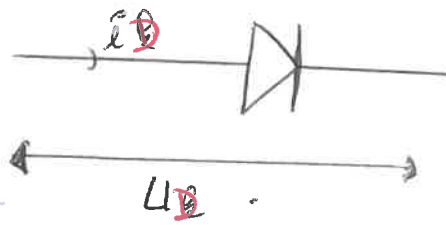
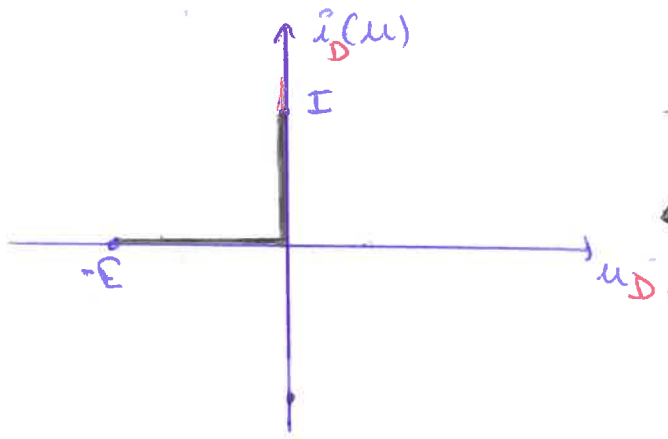


Ce circuit n'est pas possible car $i=0$ qui n'est pas possible pour une source de courant

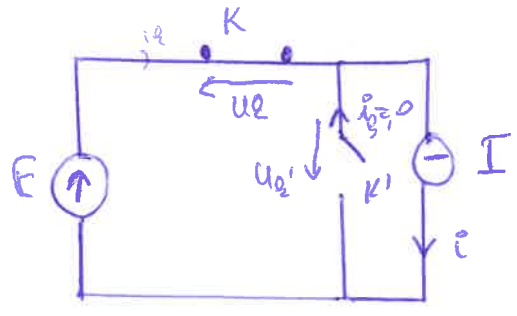
a) Pow in transistor, on a s



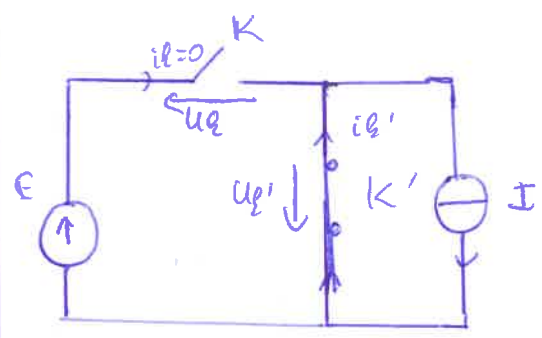
o Pow en diode, on a s



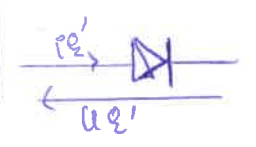
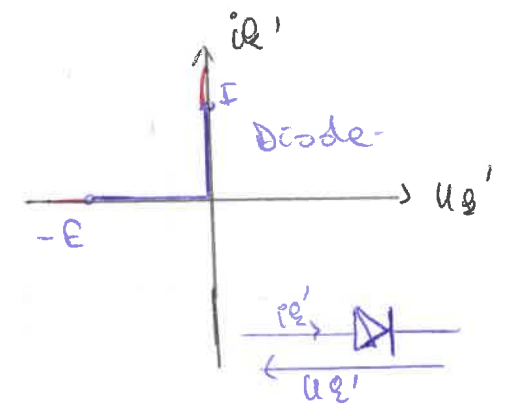
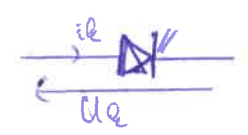
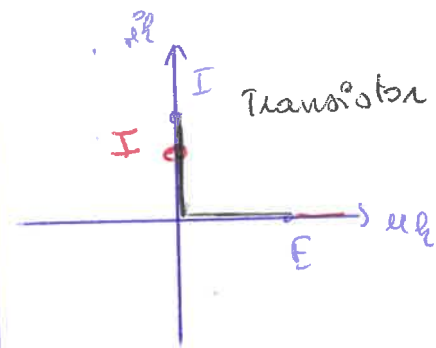
b) Pow t ∈ [0, αT]



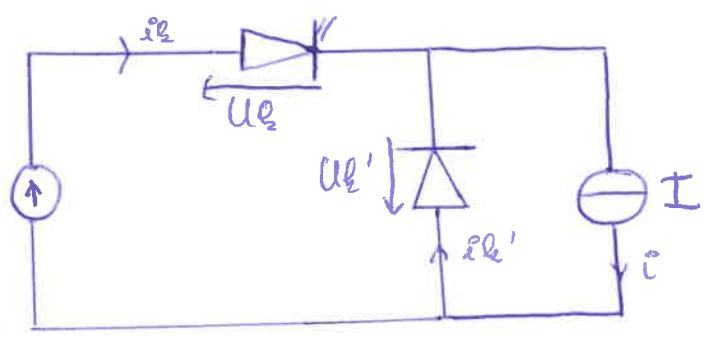
Pow t ∈ [αT, T]



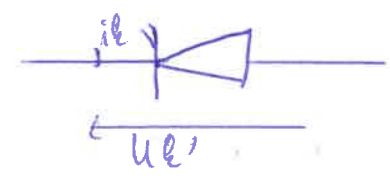
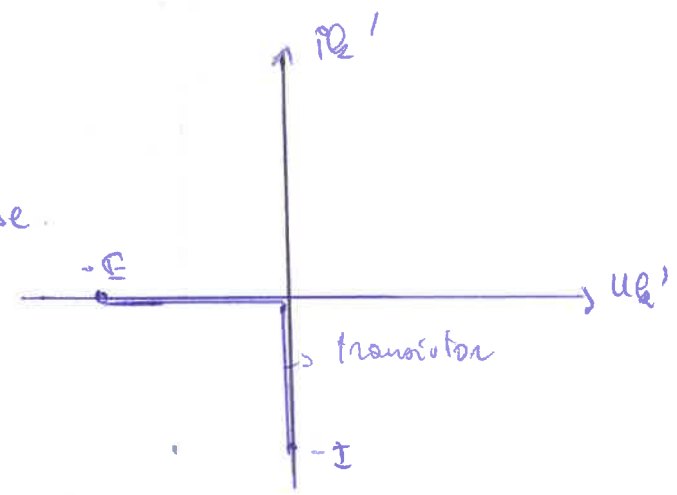
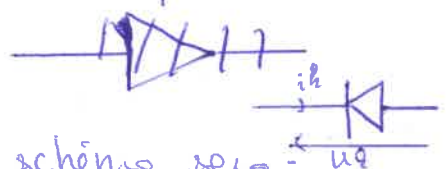
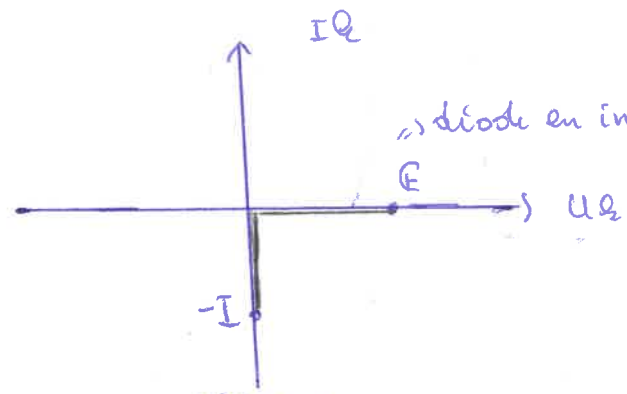
	i_Q	u_Q	i_Q'	u_Q'
$[0, IdT]$	I	0 K'bene	0	$-E$ K'ouest
$[dT, T]$	0	E K'ouest	I	0 K'bene'



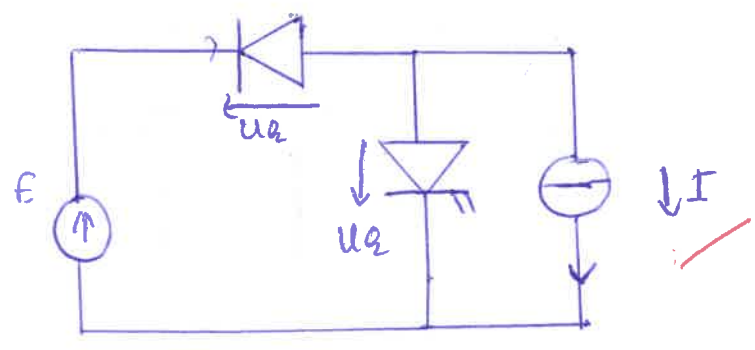
Ainsi le schéma devient



c) lorsque $i < 0$, on aura :

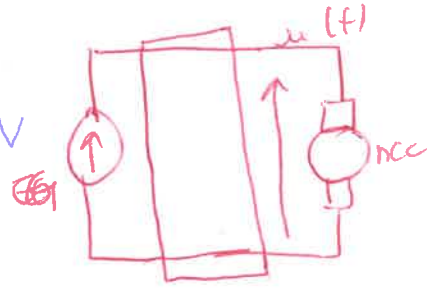
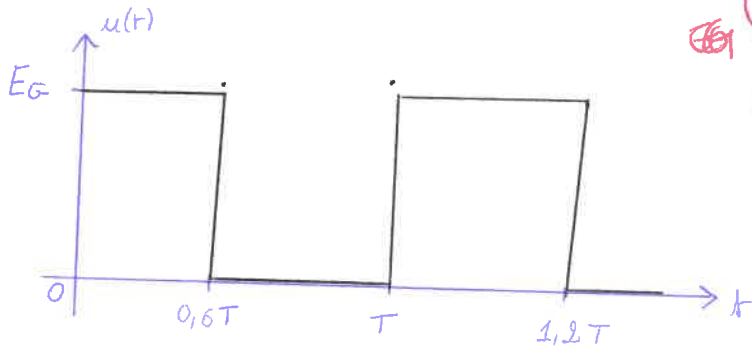


d) Ainsi le schéma sera :



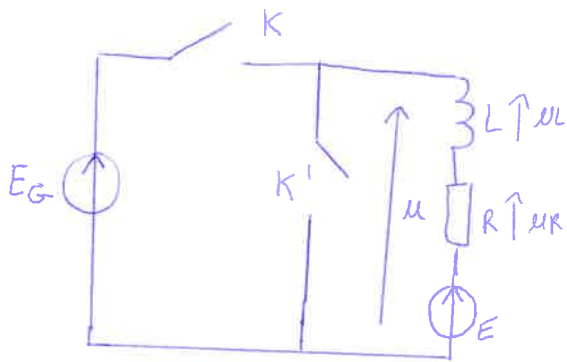
TD 30 - AD4 - (Groupe 2)

1) On a $\alpha = 0,6$ et $E_G = 150V$



tension moyenne : $\langle u(t) \rangle = \frac{1}{T} \times \text{aire sous la courbe}$
 $= \frac{1}{T} \times E_G \times \alpha T = \alpha E_G = 0,6 \times 150$
 $= 90V$

2)



3) $u(t) = E + Ri + L \frac{di}{dt}$ donc $\langle u(t) \rangle = \langle E \rangle + \langle Ri \rangle + \langle L \frac{di}{dt} \rangle$
 $= E + R \langle i(t) \rangle$

4) $\langle i(t) \rangle = \frac{\langle u(t) \rangle - E}{R} = \frac{\alpha E_G - E}{R} = \frac{90 - 80}{1,5} = 6,7 A$